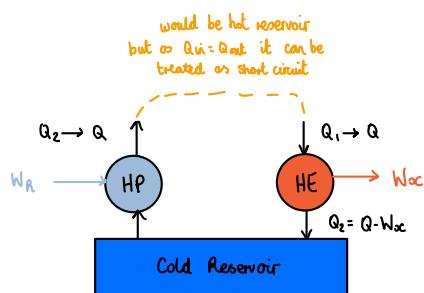


Clausius Statement

Impossible to construct device that operates in cycle and transfers heat from cooler to hotter body without work being done on system by surroundings

heat engines must exchange heat with ≥ 2 reservoirs

system exchanging heat with 1 reservoir



From Kelvin-Planck $|W_{c1}| - |W_{c2}| \leq 0$

$$|W_{c1}| < |W_{c2}|$$

heat transfer by infinitesimally small temp. differences

forces on moving boundaries only infinitesimally different from external

Reversible: when fluid undergoes process, fluid and surroundings can always be restored to original states

Reversibility

Kelvin-Planck Statement: Impossible for device operating on a cycle to receive heat from single reservoir and produce a net amount of work → engine with no heat rejection impossible

if a small amount of heat transfer, the change is negligible

Cold = sink
→ e.g. lake

does 0 work
or
accepts free work from surroundings

heat engine
Perpetual motion machine
2nd kind

Hot = source
→ e.g. sun

Reservoir

2nd Law of Thermodynamics

Claussius Inequality

$\oint \frac{dQ}{T} < 0$
equal when reversible
less than when irreversible
 $T = \text{temp of fluid supplying heat}$

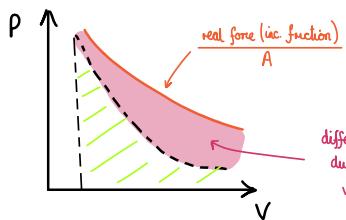
$$\frac{\delta Q_1}{T_1} + \frac{\delta Q_2}{T_2} + \dots < 0$$

Isentropic Efficiency Compressor
 $\eta = \frac{W'}{W} = \frac{h_2' - h_1}{h_2 - h_1}$
where W' means isentropic work and W is real work
Inverse

Isentropic Efficiency Turbine
 $\eta = \frac{W}{W'} = \frac{h_2 - h_1}{h_2' - h_1}$

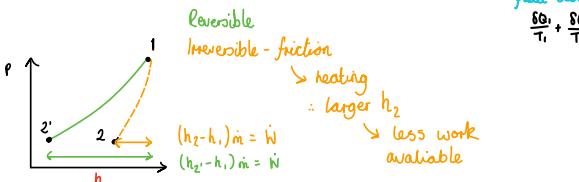
heat engine
 $1 - \eta = \frac{|Q_2|}{|Q_1|} = \frac{T_2}{T_1}$
→ Carnot Efficiency of Engine
 $\eta_C = 1 - \frac{|Q_2|}{|Q_1|} = 1 - \frac{|T_2|}{|T_1|}$

Fluid Friction



difference in work due to friction vs. ideal work

Turbine Friction



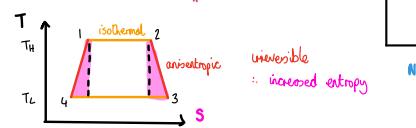
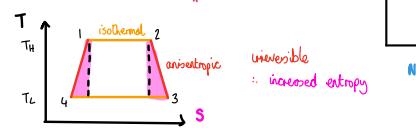
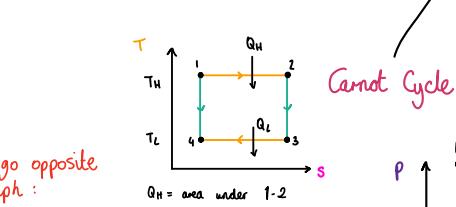
Isentropic Efficiency Turbine:

$$\eta = \frac{W}{W'} = \frac{h_2 - h_1}{h_2' - h_1}$$

inverse

for way compressor, go opposite along graph:

$$\eta = \frac{W}{W} = \frac{h_2' - h_1}{h_2 - h_1}$$



$dU = dQ_{rev} + dW_{rev} = TdS - pdV$
dividing by mT , rearranging for dS and substituting $dU = C_v dT$ and $p = \frac{RT}{V}$
then integrating:

$$S_2 - S_1 = C_v \int_{T_1}^{T_2} \frac{dT}{T} + R \int_{V_1}^{V_2} \frac{dV}{V} = C_v \ln\left(\frac{T_2}{T_1}\right) + R \ln\left(\frac{V_2}{V_1}\right)$$

$$\text{Substituting } \frac{V_2}{V_1} = \frac{T_2}{T_1} \times \frac{P_2}{P_1}$$

$$\Delta S_{12} = C_v \ln\left(\frac{T_2}{T_1}\right) + R \ln\left(\frac{P_2}{P_1}\right) + R \ln\left(\frac{P_2}{P_1}\right)$$

$$C_v + R = C_p$$

$$\Delta S_{12} = C_p \ln\left(\frac{T_2}{T_1}\right) - R \ln\left(\frac{P_2}{P_1}\right)$$

for isentropic (constant entropy)
 $S_i = S_2$

$$\therefore \frac{T_2}{T_1} = \left(\frac{P_2}{P_1}\right)^{\frac{1}{\gamma}} \quad \gamma = \frac{C_p}{C_v}$$

heat capacity ratio

For pure, incompressible liquids: $dV = 0$

distinction between C_v and C_p omitted:

$$ds = \frac{du}{T} + \beta \frac{dp}{T} = C \frac{dT}{T}$$

$$\Delta S_{12} = C \ln\left(\frac{T_2}{T_1}\right)$$